Measurement of the cutoff frequency of the electroluminescence of LEDs at low currents Viacheslav Sergeev^{1,2}, Ilya Frolov^{1,2}, Oleg Radaev¹

The purpose of the investigation. This report presents the result of an analysis of errors that occur when measuring the LEDs 3dB frequencies(cutoff frequency) at currents in the microcurrent region.

Description of the measurement technique and setup.



 $U_n = \sqrt{e^2 + 4kTR_f Df + (iR_f)^2 + 2qIR_f^2 Df}$

where I is the average value of the current flowing through the photodiode; q - electron charge, e - RMS noise voltage at the op-amp input, i - noise of the op-amp input current, the second and third terms of the expression are the thermal noise of the feedback resistor of the amplifier and the shot noise of the _photodiode, respectively.

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band D f:

The study of the dependence of the LED 3dB frequency on the current was carried out using the installation, the block diagram of which is shown in fig. 1 The LED is powered by DC, which is modulated by low amplitude AC from the output of the HP4195A network analyzer in the frequency range 0.1 - 10 MHz in frequency sweep mode. The registration of the LED optical signal is carried out by a high-speed photodectector. The electrical signal from the output of the photodetector is fed to the input of the HP4195A network analyzer, which reads the 3dB frequency value at a given LED DC current level.

Let us consider the errors due to the nonlinearity of the *P-I* characteristic when measuring 3dB frequency by detecting harmonic radiation and converting the alternating voltage of the photodiode by the root-mean-square (RMS) detector.

Based on the ABC-model of charge carrier recombination, the watt-ampere characteristic of LEDs at low currents can be approximated by the function:

 $P(I) = m(1 - \sqrt{1 + 2qI} + qI) = \frac{m}{2}(\sqrt{1 + 2qI} - 1)^{2}$ $m = \eta_{extr} V \frac{hc}{\lambda} \frac{A^2}{2B}$, $q = \frac{h_{inj}}{eV} \frac{2B}{\Lambda^2}$,

A – nonradiative recombination coefficient, B – radiative recombination coefficient.

Substituting the expressions for the coefficients in (2), (6) By adding additive noise U_n to the photodiode signal and carrying out mathematical transformations, an expression was obtained for estimating the relative error, taking into account the noise of the measuring $\varepsilon = \frac{\overleftarrow{\mathbf{e}}_{\mathbf{f}}}{\overleftarrow{\mathbf{e}}_{3}} - 1 \frac{\ddot{\mathbf{o}}_{\mathbf{f}}}{\overleftarrow{\mathbf{e}}_{3}} 100\%$ $\hat{e}_{0} \hat{e}_{2} SaI_{m} \hat{a}_{4a}^{2}$ where *S* is the power conversion coefficient of the LED into the output voltage of the photodetector, which is determined by the sensitivity of the photodiode, the gain, the radiation patterns of the LED and the photodiode and has the dimension [V/W].

For the selected elements for the transimpedance amplifier, using expression (7), the RMS value of the noise voltage at the output $U_n = 43 \,\mu\text{V}$ was calculated. Using (6), dependences of the LED 3dB frequency measurement error on the current amplitude at 1 μ A (a) and 10 μ A (b) were plotted, due to the nonlinearity of the watt-ampere characteristic of the LED and the noise of the photodetector $U_{\rm n} = 43 \,\mu\text{V}$, at $S = 20 \,\text{V/W}$ (fig. 4).









photodetector noise.

Conclusions.

The dependences of the relative errors of measuring the LED 3dB frequency on the amplitude of the test harmonic current are obtained when the alternating radiation is detected by a photodiode and the alternating voltage of the photodiode is converted by the RMS detector. It has been established that due to the nonlinearity of the *P*-*I* of the LED and in the presence of additive noise in the measuring circuit, there is an optimal value of the test current amplitude, at which the total relative measurement error takes the minimum value.

Fig. 2. *P-I* characteristics of LEDs at different values of parameter *q*: a) $q = 10^7 \text{ A}^{-1}$; b) $q = 10^5 \text{ A}^{-1}$.

Fig. 3. Measurement error of the LED 3dB frequency on the current amplitude at currents 1 μ A (a) and 10 μ A (b), due to the non-linearity of the LED *P-I* characteristic.

Fig. 4. 3dB frequency measurement error of the LED as a function of the current amplitude at a currents 1 μ A (a) and 10 μ A (b) due to the non-linearity of the LED *P*-*I* characteristic and